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<b>(54) Title:</b> FORMING A CRYSTALLINE SEMICONDUCTOR FILM ON A GLASS SUBSTRATE		
<b>(57) Abstract</b> <p>A method of forming a crystalline semiconductor film on a glass substrate is described. The method relies on heating the glass substrate to a temperature at or above its strain point during a deposition or processing of the semiconductor film. Alternatively an intermediate film of a low strain point material is deposited on the glass substrate before depositing the semiconductor material. The process relaxes stresses at temperatures above the strain point. At temperatures below the strain point, the stresses can be controlled by slow cooling and by appropriate selection of the thermal expansion coefficient. Normal soda lime glasses having low strain points may be used for the glass substrate.</p>		

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## FORMING A CRYSTALLINE SEMICONDUCTOR FILM ON A GLASS SUBSTRATE

**Introduction**

The present invention relates generally to the field of semiconductor devices and in particular the invention provides an improved method for the formation of crystalline films on glass substrates.

**Background of the Invention**

Considerable attention internationally is being directed towards developing technology for depositing polycrystalline silicon films on glass. This interest arises from the use of these films for forming electronic devices and circuits for active matrix liquid crystal displays and for use of these films in solar cells. Silicon film thickness could be in the 30 nm to 100  $\mu\text{m}$  range depending on application. For solar cell use, silicon film thickness in the 0.5-100  $\mu\text{m}$  range is of particular interest, with optimal designs likely to be in the 1-15  $\mu\text{m}$  range.

As part of these efforts, considerable attention is being directed to the development of supporting glass substrates with specific properties, particularly in relation to the thermal expansion coefficient of the glass relative to silicon and the strain point of the glass (temperature at which viscosity reaches a value of  $10^{14.5}$  poise). For example, Corning Glassworks have developed a barium alumina silicate glass known as Corning 1737 of strain point above 660°C with a thermal expansion coefficient closely matched to silicon below this temperature for use in active matrix liquid crystal displays; the Max Planck Institute in Stuttgart has developed a glass of unspecified composition which has a strain point of 820°C and a thermal expansion coefficient even better matched to silicon below this temperature for use in solar cells.

A surprising conclusion from research of the present inventors is that this earlier work is heading in the wrong direction. Because amorphous silicon shrinks irreversibly when crystallised, use of a high-strain point glass as a substrate will result in a highly stressed film prone to cracking, even if it is perfectly expansion matched. The present invention arises from the realisation by the inventors that the normal soda lime glasses, developed over the centuries largely to produce durable glass which could be manufactured at low processing temperatures, and hence having low strain points, are ideal for this application. Throughout this specification, the term 'amorphous silicon' is used to describe silicon and silicon alloys containing a high

proportion of amorphous silicon such that the material displays the shrinkage characteristic of amorphous silicon material upon its crystallisation. However, the material may include a proportion of crystalline silicon (eg Crystalitec) as well as alloying substances and  
5 impurities.

**Statement of Invention**

According to a first aspect, the present invention provides a method of forming a thin film of crystalline semiconductor material supported by a glass substrate, including the steps of:-

- 10 depositing a film of the semiconductor material in amorphous form over the glass substrate;
- processing the semiconductor material to form crystalline semiconductor material;
- during or subsequently to the processing step, heating the substrate  
15 and semiconductor material to a temperature at or above the strain point temperature of the substrate;
- subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.

20 According to a second aspect, the present invention provides a method of forming a thin film of crystalline semiconductor material supported by a glass substrate, including the steps of:-

- a) heating the glass substrate to a temperature at which deposition of the crystalline semiconductor material may occur;
- 25 b) depositing a film of the crystalline semiconductor material over the glass substrate;
- c) during or subsequently to the depositing step, heating the substrate and semiconductor material to a temperature at or above the strain point temperature of the substrate;
- 30 d) subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.

According to a third aspect, the present invention provides a method of forming a thin film of crystalline semiconductor material supported by a  
35 glass substrate, including the steps of:-

- a) heating the substrate to a temperature at or above the strain point temperature of the substrate;
- b) after the heating step and while the substrate is still at or above the strain point temperature depositing a film of the crystalline semiconductor material over the glass substrate;
- c) subsequently to the deposition step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.

According to a fourth aspect, the present invention provides a method of processing an amorphous semiconductor film supported by a glass substrate to crystallise the film, the method including the steps of:-

- a) processing the semiconductor material to form crystalline semiconductor material;
- b) during or subsequently to the processing step, heating the substrate and semiconductor material to a temperature at or above the strain point temperature of the substrate;
- c) subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.

According to a fifth aspect, the present invention also provides a method of forming a thin film of crystalline semiconductor material supported by a glass substrate, including the steps of:

- a) forming a low strain point temperature film over the substrate;
- b) depositing a film of amorphous semiconductor material over the low strain point temperature film;
- c) processing the semiconductor material film to form crystalline semiconductor material film.

According to a sixth aspect, the present invention also provides a device manufactured according to any one of the above methods.

According to a seventh aspect, the present invention further provides a semiconductor device including a film of crystalline semiconductor material formed on a glass substrate the substrate having a strain point temperature below the desired crystallisation temperature of the semiconductor material and a temperature co-efficient not less than that of the semiconductor material.

Preferably the substrate is a glass having a strain point temperature below the desired crystallisation temperature of the semiconductor material.

In this context desired crystallisation temperature is the temperature at which crystallisation occurs to achieve desired crystalline characteristics.

5 In one method according to the invention, during or after the crystallisation step the substrate is heated to a temperature where it will deform under gravity against a planar form, within a predetermined processing period, to reverse buckling caused by differential stress between the substrate and the semiconductor film. This temperature will be  
10 somewhere between the strain point and the working point of the glass, the temperature used being dependent upon the speed with which the glass is required to flatten. Using this method the substrate can also be placed on a shape form to produce purpose shaped panels for applications such as vehicle sun roofs. In the case of soda lime glass the temperature used with  
15 good effect in one embodiment of the invention is 650°C.

In another method according to the invention, during or after the crystallisation step the substrate is heated to a temperature at or above the strain point temperature but below the sagging temperature. The sagging temperature is the temperature where it will deform under gravity within a  
20 predetermined processing period. Using this alternative method films can be successfully processed with a maximum temperature of 620°C. This method may be performed with the substrate clamped to a supporting form to reduce buckling.

In another method according to the invention the cooling step  
25 includes a step of rapidly cooling the surface of the substrate carrying the semiconductor film. Preferably also the cooling step includes a step of rapidly cooling the surface of the substrate opposite to the surface carrying the semiconductor film. In this context rapid cooling is intended to indicate cooling at a rate at which the glass is not substantially isothermal whereby  
30 the glass is also tempered by the cooling process. For 3 mm soda lime glass a rate slower than in the order of 0.5°C/sec would be considered isothermal. However this value will vary according to the type of glass and its thickness. The rate will vary approximately as the square of thickness such that for 1 mm glass isothermal cooling will occur at rates slower than in the order of  
35 5°C/sec while for 10 mm thick glass isothermal cooling will occur at rates slower than in the order of 0.05°C/sec. Throughout this specification, cooling



which is referred to as greater than the rate at which isothermal cooling will occur will be taken to be at a rate at or above a rate for the particular glass thickness which corresponds to those rates given above for 1, 3 & 10 mm glass respectively, and which results in a significant temperature gradient  
5 across the thickness of the glass during the cooling process.

In the case of 3 mm soda lime glass a typical cooling rate in the region from 20°C above the strain point to 20°C below the strain point would be such that the transition took in the order of 10 seconds (ie 4°C/sec) but rates in the range 0.5°C to 10°C/sec can be applied to good effect. At  
10 temperatures further from the strain point cooling may take place at higher or lower rates depending upon other processing requirements.

In one embodiment of the invention, the surface of the substrate on which the semiconductor film is formed is modified to make it more fluid at low temperatures. The surface may be modified by the addition or removal  
15 of selected chemical species or by high energy irradiation. Alternatively a low strain point layer can be deposited onto the substrate surface prior to formation of the semiconductor film.

Preferably the semiconductor film is a film of doped or undoped silicon or silicon alloy material. In one application of the invention the  
20 silicon film is formed as a plurality of different doped layers of silicon forming one or more rectifying junctions arranged as a photovoltaic device, or solar cell.

The silicon film may be formed by methods such as plasma enhanced chemical vapour deposit or sputtering amongst others.

25 Silicon film thicknesses with a lower limit of 0.1µm can be employed in various embodiments covering a range of applications however preferably in photovoltaic applications films with a lower limit of 0.5µm and most desirably a lower limit of 1µm are employed.

A practical upper limit for film thickness is 100µm however for solar  
30 cell devices a preferred upper limit of film thickness is 15µm.

The method of invention can be performed with glasses having a strain point below the melting point of silicon, however it is more desirable that the substrate have a strain point below or at least not significantly above the desired crystallisation temperature of the silicon film (approx 600°C).

35 The best effect of the invention is achieved when the substrate has a temperature co-efficient not less than that of the crystalline semiconductor

material, at least for temperatures below the strain point temperature of the substrate.

Preferably the substrate will be soda lime glass or a similar glass having a strain point temperature at or below 520°C, an annealing point of approximately 550°C and a temperature co-efficient of 4-10ppm/°C.

Soda lime glasses with a composition of 70-75% by weight SiO<sub>2</sub>, 10-20% Na<sub>2</sub>O, 3-15% CaO and less than 0.2% by weight Fe<sub>2</sub>O<sub>3</sub> have been found to be effective in performing the invention while low iron glasses having less than 0.1% Fe<sub>2</sub>O<sub>3</sub> have been found to be particularly advantageous when the approach is used to form solar cells. Preferably, glass with a thickness in the range of 2-4 mm will be used.

In one alternative embodiment, an intermediate layer is formed between the substrate and the semiconductor film, the intermediate layer having a low strain point and a thickness in the range of 0.1-10µm. As well as providing strain relief at lower temperatures the intermediate layer can be used to act as a chemical barrier layer and/or anti reflection layer. Intermediate layers such as nitride layers, that do not contribute strain relief at low temperatures can also be included without substantially interfering with the process described.

In the embodiments described above and in the following detailed description, the glass substrate may become the superstrate in a final product. For example, in the case of a solar cell, the cell may be illuminated through the glass layer.

#### **Brief Description of the Drawings**

Embodiments of the invention will now be described in greater detail with reference to the accompanying drawings in which:

Figure 1 graphically illustrates a comparison of silicon film stress development for a high-temperature glass (Corning 1737) and a low-temperature glass (soda lime) when subjected to crystallisation of the film at a temperature of 620°C (Positive stress values indicate tensile stress and negative values indicate compressive stress);

Figures 2(a)-(d) diagrammatically illustrate four stages of processing of a silicon film on a Corning 1737 glass substrate;

Figures 3(a)-(d) diagrammatically illustrate four stages of processing of a silicon film on an unclamped soda lime glass substrate including heating to a temperature above the strain point of the substrate;

Figures 4(a)-(d) diagrammatically illustrate four stages of processing of a silicon film on a clamped soda lime glass substrate including heating to a temperature above the strain point of the substrate; and

Figures 5(a)-(e) diagrammatically illustrate five stages of processing of a silicon film on an unclamped soda lime glass substrate including heating to a temperature above the softening point of the substrate;

In these drawings, the glass substrate is assumed to be several millimetres thick so that at temperatures below the strain point, deformation due to elastic stress is negligible. If the glass were very thin, typically less than 1 mm, then the glass would develop a curvature caused by residual stress at the end of the process. For compressive stress in the film, the glass would bend away from the film side, while for tensile stress, the glass would bend toward the film side.

#### **Detailed Description of Embodiments of the Invention**

The invention will now be described in detail with specific examples using soda lime glass and with reference to Corning 1737 glass by way of comparison, however the invention is equally applicable to other low temperature glasses.

#### **Normal Sequence**

For polycrystalline silicon active matrix liquid crystal displays, silicon is normally deposited in amorphous form onto a high strain point glass substrate such as Corning 1737. The amorphous silicon is then crystallised without exceeding the temperature of the strain point of the glass either by prolonged heating at low temperature in a furnace or with very short high intensity pulses from a light source such as a laser which result in minimal heating of the glass. Sometimes both of these steps are applied sequentially. The resulting polycrystalline material is then processed into the desired electronic device. By minimising the thermal expansion difference between the glass and the silicon, stresses due to thermal expansion mismatch can be minimised throughout the processing. Since the thermal expansion coefficient of the glass increases greatly once heated above its strain point and the glass can distort above these temperatures, it has been thought important that the strain point not be exceeded during this processing. But, despite this precaution, strong tensile stress is induced in the film due to irreversible shrinkage that occurs during crystallisation.

### Film Contraction Upon Crystallisation

Prior art approaches to developing silicon films can only poorly accommodate the contraction of the originally amorphous silicon layer upon crystallisation. Typically, the volume of an amorphous film is 1-3% larger than that of its crystalline counterpart due to the more compact organisation of atoms in the latter. If using a glass with a thermal expansion coefficient matched to silicon, the contraction of the silicon upon crystallisation will create an undesirable tensile stress in the film. This makes the film susceptible to cracking, particularly if it is reasonably thick.

### Improved Process

The improved process employed in embodiments of the present invention relies on deliberately heating the glass substrate above its strain point during processing making the low temperature glasses, such as soda lime glasses, ideal for this use. Since the glass is plastic above this temperature while the silicon remains elastic, the glass is forced to conform to the shape defined by the silicon once this temperature is exceeded. This process relaxes any stresses which might otherwise be created in the glass or film, as long as the glass temperature is above the strain point. As the glass temperature is reduced back below the strain point, the glass becomes progressively more rigid and stresses will begin to build up in the film and glass.

If cooled slowly, the stress in the film and the glass can be controlled by appropriate selection of its thermal expansion coefficient relative to that of silicon, particularly those with linear expansion coefficients in the range 4-10 ppm/°C below the strain point. Particularly interesting are glasses with thermal expansion coefficients higher than silicon. Slow cooling will result in a compressive stress in the silicon film which is desirable from the point of view of its mechanical integrity, particularly in relation to a significantly reduced potential for film cracking.

The amount of stress left in the film can be controlled by the rate of cooling. In particular, fast cooling of the film will leave the high temperature structure of the glass frozen into the surface layer, allowing a controlled amount of compressive stress to be generated in the thin film. Simultaneous fast cooling of the opposite glass surface will leave a similar high temperature structure remaining in the glass and leave this surface in compression. The more slowly cooling central regions of the glass layer will

be in tension due to the greater contraction of these more slowly cooling regions. This arrangement is particularly desirable for maximising the tolerance of the entire structure to cracking.

Conversely, by choosing a glass with a low strain point, the  
5 crystallisation process occurs at a temperature where the glass is soft. The contraction within the silicon film is accommodated by the deformation of the soft glass, removing the tendency for the films to crack and allowing the processing of thick films.

#### **Alternative implementations**

10 The previous effects could be enhanced by incorporating additional processing features. For example, the surface of the glass onto which the film is to be deposited could be made softer and more easily deformable at low temperatures by several approaches. One could be by chemical  
15 modification of the glass such as by the incorporation of additional chemical species or by the removal of selected species from the surface region of the glass. Another may be by surface modification by high energy particle irradiation. This is known to increase the ability of the glass to deform in response to stresses at low temperatures. Alternatively, a low strain point layer could be deposited onto the glass surface prior to the deposition of the  
20 silicon film to produce these benefits at even lower temperature than would be possible using uncoated glass.

#### **Experimental Results**

Amorphous silicon films have been deposited by several techniques onto both low temperature soda lime glass and higher temperature barium  
25 alumina silicate glass (Corning 1737). Films deposited by plasma enhanced chemical vapour deposition have been observed to have an intrinsic compressive stress after deposition as do those deposited by sputtering. This intrinsic stress tends to mildly distort thin glass substrates which are generally elastic at the low deposition temperatures involved. The amount of  
30 stress can be measured by measuring the very slight curvature imparted to the glass sheet. Typical values of intrinsic stress combined with the thermal expansion mismatch stress arising from cooling from the deposition temperature to room temperature are in the range 100-600 megapascals (MPa). Other deposition techniques might give rise to different stresses  
35 without any impact upon the effectiveness of the approach described. Upon heating, the higher thermal expansion coefficient of the soda lime glass will

tend to reduce this compressive stress in the deposited film and even make it tensile, while it will remain virtually unchanged in the barium alumina silicate glass due to its good thermal expansion match to silicon.

If heated to a crystallisation temperature which is above the strain point of the soda lime glass, stresses in the film will relax by glass deformation. The glass will physically deform to adjust its shape to that of the zero stress silicon film. Upon crystallisation, the glass similarly adjusts to the reduced dimensions of the crystallised film. Upon cooling, a compressive stress will build up in the film due to its smaller expansion coefficient compared to that of the much thicker glass substrate. The amount of stress can be controlled by the cooling rate as previously mentioned.

In the case of the higher strain point temperature glass, the silicon film will go into tension when it contracts on crystallisation. This can create cracking in films. Cracking has been observed in films thicker than 4 microns when deposited upon such glass. This tensile stress remains after cooling due to the thermal expansion match during the cooling process. The stresses will not be able to be modified to the same extent by controlling the cooling rate.

#### Computer Simulations

The interpretation of the experimental results has been aided by the use of the computer simulation package ABAQUS. The general variation of stress in the silicon film as a function of time for thin silicon films deposited onto both high temperature glass with a thermal expansion coefficient matched to silicon (Corning 1737), such as conventionally used in these applications, and a low temperature soda lime glass is shown in Figure 1.

For the case simulated, the silicon films are deposited onto one side of the glass substrates at relatively low temperature in amorphous form, then cooled to room temperature, the starting point in Figure 1. The film and substrate are then heated to a temperature sufficiently large to allow the amorphous silicon films to crystallise. This temperature is intermediate between the strain points of the low temperature glass and the high temperature glass. After crystallisation is complete, the samples are cooled to room temperature.

The silicon films are generally deposited at intermediate temperatures in the range of 200 - 500°C. An intrinsic stress is produced in the films during deposition with the magnitude and sign of this stress

depending upon the nature of the deposition process and the deposition parameters. For the case of Figure 1, a compressive intrinsic stress is modelled as frequently observed in experimental films. Stress development has been modelled in Figure 1 for both Corning 1737 and soda lime glass, with an initial compressive intrinsic stress of -300 MPa at the deposition temperature of the amorphous film.

During cooling to room temperature after deposition, there will be a change in stress levels depending on the relative thermal expansion coefficients of the silicon film and the glass. The stress in the film on the low temperature soda lime glass will become more compressive (approx -700MPa) than that of the film on the high temperature glass (approx. -350 MPa) due to the much higher thermal expansion coefficient of the former.

During heating to the crystallisation temperature of the film, the stress in the film on the soda lime glass will become more tensile, again due to its lower thermal expansion coefficient than the glass, reaching its maximum tensile value, as shown on Figure 1. This maximum is attained since the glass viscosity decreases as it is heated, with the glass becoming quite soft and able to relax its structure to accommodate the stress at temperatures above the strain point. The stress in the high temperature Corning 1737 glass will vary only slightly from its room temperature value during the heating stage since the glass is designed to have a similar thermal expansion coefficient to silicon.

The amorphous silicon then begins to crystallise. The compaction of the silicon upon crystallisation will tend to be restrained by the glass producing tensile stresses in the film. This is very apparent in the case of the high temperature glass (Corning 1737) of Figure 1. The compressive intrinsic stress after deposition converts to a tensile stress during film crystallisation. However, since the low temperature soda lime glass is above its strain point during crystallisation, it is unable to restrain the compaction of the film. Hence, there is very little increase in the tensile stress in the film during crystallisation in this case.

After crystallisation, the film and substrate are cooled to room temperature. For the high temperature glass (Corning 1737), there will be little change in stress levels in the film during cooling since its thermal expansion coefficient is matched to silicon. However, as the soda lime glass cools below its strain point, it becomes more rigid and the higher thermal

expansion coefficient of the glass causes the residual tensile stress in the film to become compressive.

Referring to Figures 2-6 five processes discussed above will be described to examine the stresses existing in a silicon film during raised temperature processing on a glass substrate. Turning firstly to Figure 2 this series of diagrams shows stress exhibited in a silicon film deposited on a Corning 1737 glass substrate at the following points in a processing sequence, neglecting the slight curvature of the glass caused by the elastic stress described:

- 2(a) Compressive stress in the amorphous silicon film prior to heating (20°C);
- 2(b) Compressive stress in the amorphous silicon at 620°C prior to crystallisation;
- 2(c) Tensile stress in the silicon film at 620°C after crystallisation;
- and
- 2(d) Tensile stress in the crystalline silicon film at 20°C after cooling.

Because Corning 1737 glass has not reached its strain point at 620°C the compressive stresses shown in figure 2(b) and the tensile stresses shown in figure 2(c) are not relieved. Further, because this glass has a temperature co-efficient which is closely matched to silicon the tensile stress present at 620°C in figure 2(c) is still present when the substrate and film has been cooled to 20°C. Therefore it will be noted that this glass is not suitable for the process of the present invention as the detrimental tensile stress in the silicon film is not relaxed and remains at the end of the processing sequence.

In figure 3 the same processing points are illustrated as in Figure 2, but in this case the substrate is soda lime glass and the conditions are as follows:-

- 3(a) Compressive stress in the amorphous silicon film prior to heating (20°C);
- 3(b) Due to the higher temperature co-efficient of soda lime glass, tensile stress has developed in the amorphous silicon film as it is heated to 620°C but prior to crystallisation of the silicon, however the soda lime glass has passed its strain point and bending occurs with significant resultant relief of the tensile stress in the silicon film leaving only a residual stress level remaining;



3(c) After crystallisation at 620°C the silicon film has contracted but the tensile stress in the film has only increased slightly as the glass has absorbed some of the contraction, resulting in a similar residual stress level to that of Figure 3(b).

- 5        3(d) Cooling of the substrate has frozen the bend in the glass as the temperature passed through the strain point of the glass but at 20°C the silicon now exhibits a significant compressive stress due to the higher temperature co-efficient of the glass over the silicon.

10        As opposed to the case with high temperature glass in figure 2, the same processing sequence using low temperature glass results in stress relief when the glass is raised above its strain point, with the end result that the silicon film is in compression when the substrate is cooled back to 20°C.

15        The sequence illustrated in figure 4 is similar to that of figure 3 except that in this case the edges of the substrate are clamped to prevent the bending that was observed in Figures 3(a), 3(c) and 3(d).

20        In the sequence of figure 4, some buckling in the centre of the substrate is observed to be introduced at figure 4(b) and is retained in figures 4(c) and 4(d) but otherwise the stresses are seen to be substantially equal to those in the sequence of figure 3. In the diagrams of Figure 4 the buckling has been exaggerated for ease of understanding but in reality the buckling will be much less pronounced than the bending described with reference to Figure 3.

25        Turning to figure 5, this sequence is again performed on a silicon film formed on a soda lime glass substrate, with steps 5(a), 5(b) and 5(c) being as for figure 3. However in the sequence of figure 5, the additional step illustrated as 5(d) is performed, where the silicon and substrate are heated to 650°C at which point the glass has softened sufficiently to completely relieve the stress in the silicon, while allowing the glass to flatten under the effect of gravity. Cooling of the substrate then results in the figure 5(e) situation  
30        where at 20°C the silicon is again in compression but the substrate is substantially flat.

35        Other mounting arrangements for the glass can obviously be used to control the distortion of the glass during the thermal processing. For example, turning the film side of the glass downwards (i.e. supporting the panel on the film side) will accelerate the flattening of the distortion in connection with Figure 5. Constraining the glass by methods other than

pinning at the corners could completely eliminate distortion while giving the full benefits of the invention.

### Effects Of Stresses

5 There are several potentially undesirable consequences of large stresses in the film including glass distortion, film delamination and film cracking.

The first two depend upon many factors including the stress levels in the film, but will become more likely with increasing film thickness. Film cracking is likely when there is a high tensile stress in the films.  
10 Experimentally, cracking has been observed in films when over 4 microns in thickness when deposited onto high temperature Corning 1737 glass and crystallised, even when initially deposited by techniques such as sputtering which result in a high initial compressive stress in the film.

For the low temperature glass, the maximum film tensile stress  
15 occurs as the film is heated to the crystallisation temperature. This stress can be controlled in a number of ways. Control of the heating conditions will allow the use of glass relaxation to minimise the peak value. Prior thermal treatments of the glass which tend to freeze-in a high temperature structure will restrict the tendency for the glass to expand at an increased rate past the  
20 strain point temperature. Deposition of the amorphous film with a high compressive stress and at increased temperature will also reduce this maximum tensile stress.

If the low temperature soda lime glass is not constrained at this stage of the processing, distortion of the glass by bending up at the corners can  
25 occur to reduce this tensile stress. This distortion can remain through the subsequent thermal cycle. Constraining the glass at the corners prevents this occurring, with a slight buckling of the glass near its centre the only undesirable consequence. Other methods of constraint, such as more uniform loading, could reduce this distortion further.

30 Alternatively, or in conjunction with such constraints, the deformed glass can be heated to a higher temperature after film crystallisation. The glass will become even softer at such temperatures, allowing gravity to flatten the glass as confirmed by both experimentation and ABAQUS modelling. With rapid subsequent cooling of the glass surfaces, they can also  
35 allow the high temperature structure of the glass to be frozen into the glass near the surface, providing a toughening effect as in normal glass tempering.

This high temperature step could be integral with the crystallisation step or be conducted subsequently.

### Advantages

Due to their lower fabrication temperatures and the very large  
5 existing volume of production, the lower strain point high thermal expansion  
coefficient soda lime glasses are considerably lower in cost than those of the  
higher temperature thermally matched glasses. Much tighter control over the  
purity of the elements used to form the latter glasses is also required.  
Additionally, there is less scope for controlling the stress in the final silicon  
10 film by manipulation of cooling rates. The high thermal expansion  
coefficient glasses also leave the silicon films in a compressive state, which  
is desirable from mechanical aspects. The use of these glasses also allows a  
compressive stress to be built into the uncoated surface of the glass which  
will improve the durability of the film/glass composite in the field.

15 Although the advantages have been described in relation to silicon  
that is deposited in amorphous form, other techniques for depositing silicon  
will also benefit from these advantages. Specifically, films deposited directly  
in polycrystalline form at high temperature will only have stress arising from  
thermal expansion mismatch from the strain as the glass is cooled below the  
20 strain point. These considerations make it unnecessary to use expensive  
glasses for the deposition of these films which could have a major impact on  
both the cost of displays and solar cells.

Specifically, one preferred choice of glass would be the soda lime  
glasses produced in high volume with a composition containing primarily 70-  
25 75% by weight of  $\text{SiO}_2$ , 10-20%  $\text{Na}_2\text{O}$ , and 3-15%  $\text{CaO}$  and with an  $\text{Fe}_2\text{O}_3$   
composition of less than 0.2% by weight. Low iron soda lime glass with an  
 $\text{Fe}_2\text{O}_3$  composition of less than 0.1% is particularly attractive.

Silicon film thickness could be in the 30nm to 100  $\mu\text{m}$  range  
depending on application. For solar cell use, silicon film thickness in the  
30 1-100  $\mu\text{m}$  range is of particular interest, with optimal designs likely to lie in  
the 3-15  $\mu\text{m}$  range.

Strain points of the standard soda lime glasses lie in the 500-520°C  
range. Processing above the strain point will give the desirable stress  
relaxation effects noted. Crystallisation of the silicon can most effectively be  
35 conducted in the 530-650°C range, with longer crystallisation times required  
at the lower temperatures. Temperature treatment at around 650°C is

sufficiently high for gravity to remove glass distortion in reasonable times. Even higher temperature treatment will further improve the quality of the crystallised films.

5 These temperatures would be modified in ways obvious to those skilled in the art for glasses other than standard soda lime glasses where stress relaxation benefits were sought and for cases where surface modification or surface films were used to achieve similar benefits.

10 It will be appreciated by persons skilled in the art that numerous variations and/or modifications may be made to the invention as shown in the specific embodiments without departing from the spirit or scope of the invention as broadly described. The present embodiments are, therefore, to be considered in all respects as illustrative and not restrictive.

## CLAIMS:

1. A method of processing an amorphous semiconductor film supported by a glass substrate to crystallise the film, the method including the steps of:-

a) processing the semiconductor material to form crystalline

5 semiconductor material;

b) during or subsequently to the processing step, heating at least the region of the substrate adjacent to the interface between the substrate and semiconductor material to a temperature at or above the strain point temperature of the substrate;

10 c) subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.

2. A method of forming a thin film of crystalline semiconductor material directly onto a glass substrate or over an intermediate layer supported by the glass substrate, including the steps of:-

15

a) heating the glass substrate to a temperature at which deposition of the crystalline semiconductor material may occur;

b) depositing a film of the crystalline semiconductor material over the glass substrate;

20

c) during or subsequently to the depositing step, heating at least the region of the substrate adjacent to the interface between the substrate and semiconductor material to a temperature at or above the strain point temperature of the substrate;

d) subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.

25

3. The method as claimed in claim 1 or 2, wherein the semiconductor carrying surface is modified by the addition of a low strain point temperature film over the surface before the semiconductor film is deposited.

30

4. A method of forming a thin film of crystalline semiconductor material supported by a glass substrate, including the steps of:

a) forming a low strain point temperature film over the substrate;

b) depositing a film of amorphous semiconductor material over the low strain point temperature film;

35

c) processing the semiconductor material film to form crystalline semiconductor material film.

5. The method as claimed in claims 1 or 4, wherein the step of processing the amorphous semiconductor material film includes heating the film to a temperature at which solid phase crystallisation will occur.
6. The method of any one of claims 3 or 4 or 5, wherein the  
5 intermediate film has a thickness of 0.1-10 $\mu$ m.
7. The method of claim 6, wherein the intermediate film acts as a chemical barrier.
8. The method of claim 6, wherein the intermediate film acts as an anti-reflection layer.
- 10 9. The method as claimed in any one of the preceding claims, wherein the surface of the substrate supporting the semiconductor film is modified to make it more fluid at low temperatures.
10. The method as claimed in claim 6, wherein the surface of the substrate carrying surface is modified by the addition or removal of selected  
15 species.
11. The method of claim 6, wherein the semiconductor carrying surface is modified by high energy irradiation.
12. The method as claimed in any one of the preceding claims, wherein the substrate is a glass having a strain point temperature below a temperature  
20 at which the processing occurs to cause crystallisation of the semiconductor material.
13. The method as claimed in any one of the preceding claims, wherein during or after the crystallisation step, the substrate is heated to a temperature at which it will deform under gravity against a planar form,  
25 within a predetermined processing period, to reverse buckling caused by differential stress between the substrate and the semiconductor film.
14. The method as claimed in any one of claims 1 to 12, wherein during or after the crystallisation step, the substrate is heated to a temperature at which it will deform under gravity against a shaped form, within a  
30 predetermined processing period, to reverse buckling caused by differential stress between the substrate and the semiconductor film and to form the substrate to a shape determined by an end use of the device formed from the semiconductor layer.
15. The method of claim 13 or 14, wherein the substrate is heated to a  
35 maximum temperature between the strain point and the working point of the substrate.

16. The method as claimed in any one of the preceding claims, wherein the substrate is low temperature glass.

17. The method of claim 16, wherein the substrate is soda lime glass.

18. The method of claim 17, wherein the substrate is heated to a

5 maximum temperature of 650°C.

19. The method as claimed in any one of claims 1 to 14, wherein the substrate is heated to a maximum temperature which is between the strain point and the sagging temperature of the substrate.

20. The method of claim 19, wherein the substrate is clamped at its edges  
10 at least while it is heated above the strain point and during the subsequent cooling step.

21. The method as claimed in any one of claims 1 to 14, or claim 19 or claim 20, wherein the substrate is low temperature glass.

22. The method of claim 21, wherein the substrate is soda lime glass.

15 23. The method as claimed in claim 22, wherein the substrate is heated to a maximum temperature of 620°C.

24. The method as claimed in any one of the preceding claims wherein the substrate is 1 - 10 mm thick.

25. The method as claimed in claim 24, wherein the substrate is 1-5 mm  
20 thick.

26. The method of claim 25 wherein the substrate is 2-4 mm thick.

27. The method as claimed in any one of the preceding claims wherein the surface of the substrate carrying the semiconductor film is cooled from the maximum temperature to below the strain point at a rate greater than the  
25 maximum rate at which isothermal cooling can occur.

28. The method as claimed in claim 24, wherein the surface carrying the semiconductor film is cooled from the maximum temperature to below the strain point at a rate greater than the maximum rate at which isothermal cooling can occur.

30 29. The method as claimed in claim 24 or 25, wherein the rate of cooling from the maximum temperature to below the strain point is in the range of 0.1°C/sec to 10°C/sec.

30 30. The method as claimed in claim 29, wherein the rate of cooling from the maximum temperature to below the strain point is in the range of  
35 0.5°C/sec to 10°C/sec.

31. The method as claimed in claim 29, wherein the rate of cooling from the maximum temperature to below the strain point is in the order of  $4^{\circ}\text{C}/\text{sec}$ .
32. The method as claimed in any one of the preceding claims, wherein the semiconductor film is a film of material selected from doped or undoped silicon or silicon alloy.
33. The method as claimed in any one of the preceding claims, wherein the silicon film is formed as a plurality of different doped layers of silicon forming one or more rectifying junctions arranged as a photovoltaic device or solar cell.
34. The method as claimed in any one of claims 1 to 33, wherein the lower limit of semiconductor film thickness is  $0.1\mu\text{m}$ .
35. The method as claimed in any one of claims 1 to 33, wherein the lower limit of semiconductor film thickness is  $0.5\mu\text{m}$ .
36. The method as claimed in any one of claims 1 to 33, wherein the lower limit of semiconductor film thickness is  $1\mu\text{m}$ .
37. The method as claimed in any one of claims 1 to 36, wherein the upper limit of semiconductor film thickness is  $100\mu\text{m}$ .
38. The method as claimed in any one of claims 1 to 36, wherein the upper limit of semiconductor film thickness is  $15\mu\text{m}$ .
39. The method as claimed in any one of the preceding claims, wherein the strain point of the substrate is below or not significantly above the crystallisation temperature of the silicon film.
40. The method as claimed in any one of the preceding claims, wherein the substrate has a strain point at or below  $520^{\circ}\text{C}$ .
41. The method of claim 40, wherein the substrate has an annealing point of  $550^{\circ}\text{C}$ .
42. The method of claim 40 or 41, wherein the substrate has a temperature co-efficient of  $4\text{-}10\text{ppm}/^{\circ}\text{C}$ .
43. The method as claimed in any one of the preceding claims, wherein the substrate is soda lime glass with a composition of 70-75% by weight  $\text{SiO}_2$ , 10-20%  $\text{Na}_2\text{O}$ , 3-15%  $\text{CaO}$  and less than 0.2% by weight  $\text{Fe}_2\text{O}_3$ .
44. The method as claimed in claim 43, wherein the composition has less than 0.1% by weight  $\text{Fe}_2\text{O}_3$ .
45. A device manufactured by using a method as claimed in any one of the preceding claims.



46. A semiconductor device including a film of crystalline semiconductor material formed on a glass substrate the substrate having a strain point temperature below the desired crystallisation temperature of the semiconductor material and a temperature co-efficient not less than that of the semiconductor material, the device being manufactured using a method as claimed in any one of claims 1 to 44.
- 5

**AMENDED CLAIMS**

[received by the International Bureau on 6 March 1998 (06.03.98);  
original claims 1-46 replaced by amended claims 1-45 (4 pages)]

1. A method of processing an amorphous semiconductor film supported by a glass substrate to crystallise the film, the method including the steps of:-
  - a) processing the semiconductor material to form crystalline semiconductor material;
  - b) during or subsequently to the processing step, heating at least the region of the substrate adjacent to the interface between the substrate and semiconductor material to a temperature at or above the strain point temperature of the substrate so as to substantially relax stress in the film;
  - c) subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.
2. A method of forming a thin film of crystalline semiconductor material directly onto a glass substrate or over an intermediate layer supported by the glass substrate, including the steps of:-
  - a) heating the glass substrate to a temperature at which deposition of the crystalline semiconductor material may occur;
  - b) depositing a film of the crystalline semiconductor material over the glass substrate;
  - c) during or subsequently to the depositing step, heating at least the region of the substrate adjacent to the interface between the substrate and semiconductor material to a temperature at or above the strain point temperature of the substrate so as to substantially relax stress in the film;
  - d) subsequently to the heating step, cooling the substrate and semiconductor material to a temperature below the strain point of the substrate.
3. The method as claimed in claim 1, wherein the step of processing the amorphous semiconductor material film includes heating the film to a temperature at which solid phase crystallisation will occur during the period it is heated to this temperature.
4. The method as claimed in claim 1, 2 or 3, wherein the semiconductor carrying surface is modified by the addition of a low strain point temperature film over the surface before the semiconductor film is deposited.
5. The method of claim 4, wherein the intermediate film has a thickness of 0.1-10 $\mu$ m.

6. The method of claim 5, wherein the intermediate film acts as a chemical barrier.
7. The method of claim 6, wherein the intermediate film acts as an anti-reflection layer.
- 5 8. The method as claimed in claim 5, wherein the surface of the substrate carrying surface is modified by the addition or removal of selected species.
9. The method of claim 5, wherein the semiconductor carrying surface is modified by high energy irradiation.
- 10 10. The method as claimed in any one of the preceding claims, wherein the surface of the substrate supporting the semiconductor film is modified to make it more fluid at low temperatures.
11. The method as claimed in any one of the preceding claims, wherein the substrate is a glass having a strain point temperature below a temperature at which the processing occurs to cause crystallisation of the semiconductor material.
- 15 12. The method as claimed in any one of the preceding claims, wherein during or after the crystallisation step, the substrate is heated to a temperature at which it will deform under gravity against a planar form, within a predetermined processing period, to reverse buckling caused by differential stress between the substrate and the semiconductor film.
- 20 13. The method as claimed in any one of claims 1 to 11, wherein during or after the crystallisation step, the substrate is heated to a temperature at which it will deform under gravity against a shaped form, within a predetermined processing period, to reverse buckling caused by differential stress between the substrate and the semiconductor film and to form the substrate to a shape determined by an end use of the device formed from the semiconductor layer.
- 25 14. The method of claim 12 or 13, wherein the substrate is heated to a maximum temperature between the strain point and the working point of the substrate.
- 30 15. The method as claimed in any one of the preceding claims, wherein the substrate is low temperature glass.
16. The method of claim 15, wherein the substrate is soda lime glass.
- 35 17. The method of claim 16, wherein the substrate is heated to a maximum temperature of 650°C.

18. The method as claimed in any one of claims 1 to 13, wherein the substrate is heated to a maximum temperature which is between the strain point and the sagging temperature of the substrate.
19. The method of claim 18, wherein the substrate is clamped at its edges at least while it is heated above the strain point and during the subsequent cooling step.
20. The method as claimed in any one of claims 1 to 13, or claim 18 or 19, wherein the substrate is low temperature glass.
21. The method of claim 20, wherein the substrate is soda lime glass.
22. The method as claimed in claim 21, wherein the substrate is heated to a maximum temperature of 620°C.
23. The method as claimed in any one of the preceding claims wherein the substrate is 1 - 10 mm thick.
24. The method as claimed in claim 23, wherein the substrate is 1-5 mm thick.
25. The method of claim 24, wherein the substrate is 2-4 mm thick.
26. The method as claimed in any one of the preceding claims wherein the surface of the substrate carrying the semiconductor film is cooled from the maximum temperature to below the strain point at a rate greater than the maximum rate at which isothermal cooling can occur.
27. The method as claimed in claim 23, wherein the surface carrying the semiconductor film is cooled from the maximum temperature to below the strain point at a rate greater than the maximum rate at which isothermal cooling can occur.
28. The method as claimed in claim 23 or 24, wherein the rate of cooling from the maximum temperature to below the strain point is in the range of 0.1°C/sec to 10°C/sec.
29. The method as claimed in claim 28, wherein the rate of cooling from the maximum temperature to below the strain point is in the range of 0.5°C/sec to 10°C/sec.
30. The method as claimed in claim 28, wherein the rate of cooling from the maximum temperature to below the strain point is in the order of 4°C/sec.
31. The method as claimed in any one of the preceding claims, wherein the semiconductor film is a film of material selected from doped or undoped silicon or silicon alloy.

32. The method as claimed in any one of the preceding claims, wherein the silicon film is formed as a plurality of different doped layers of silicon forming one or more rectifying junctions arranged as a photovoltaic device or solar cell.
- 5 33. The method as claimed in any one of claims 1 to 32, wherein the lower limit of semiconductor film thickness is  $0.1\mu m$ .
34. The method as claimed in any one of claims 1 to 32, wherein the lower limit of semiconductor film thickness is  $1.0\mu m$ .
35. The method as claimed in any one of claims 1 to 32, wherein the lower  
10 limit of semiconductor film thickness is  $3\mu m$ .
36. The method as claimed in any one of claims 1 to 35, wherein the upper limit of semiconductor film thickness is  $100\mu m$ .
37. The method as claimed in any one of claims 1 to 35, wherein the upper limit of semiconductor film thickness is  $15\mu m$ .
- 15 38. The method as claimed in any one of the preceding claims, wherein the strain point of the substrate is below or not significantly above the crystallisation temperature of the silicon film.
39. The method as claimed in any one of the preceding claims, wherein the substrate has a strain point at or below  $520^{\circ}C$ .
- 20 40. The method of claim 39, wherein the substrate has an annealing point of  $550^{\circ}C$ .
41. The method of claim 39 or 40, wherein the substrate has a temperature co-efficient of  $4-10\text{ppm}/^{\circ}C$ .
42. The method as claimed in any one of the preceding claims, wherein  
25 the substrate is soda lime glass with a composition of 70-75% by weight  $SiO_2$ , 10-20%  $Na_2O$ , 3-15%  $CaO$  and less than 0.2% by weight  $Fe_2O_3$ .
43. The method as claimed in claim 42, wherein the composition has less than 0.1% by weight  $Fe_2O_3$ .
44. A device manufactured by using a method as claimed in any one of the  
30 preceding claims.
45. A semiconductor device including a film of crystalline semiconductor material formed on a glass substrate the substrate having a strain point temperature below the desired crystallisation temperature of the semiconductor material and a temperature co-efficient not less than that of  
35 the semiconductor material, the device being manufactured using a method as claimed in any one of claims 1 to 43.

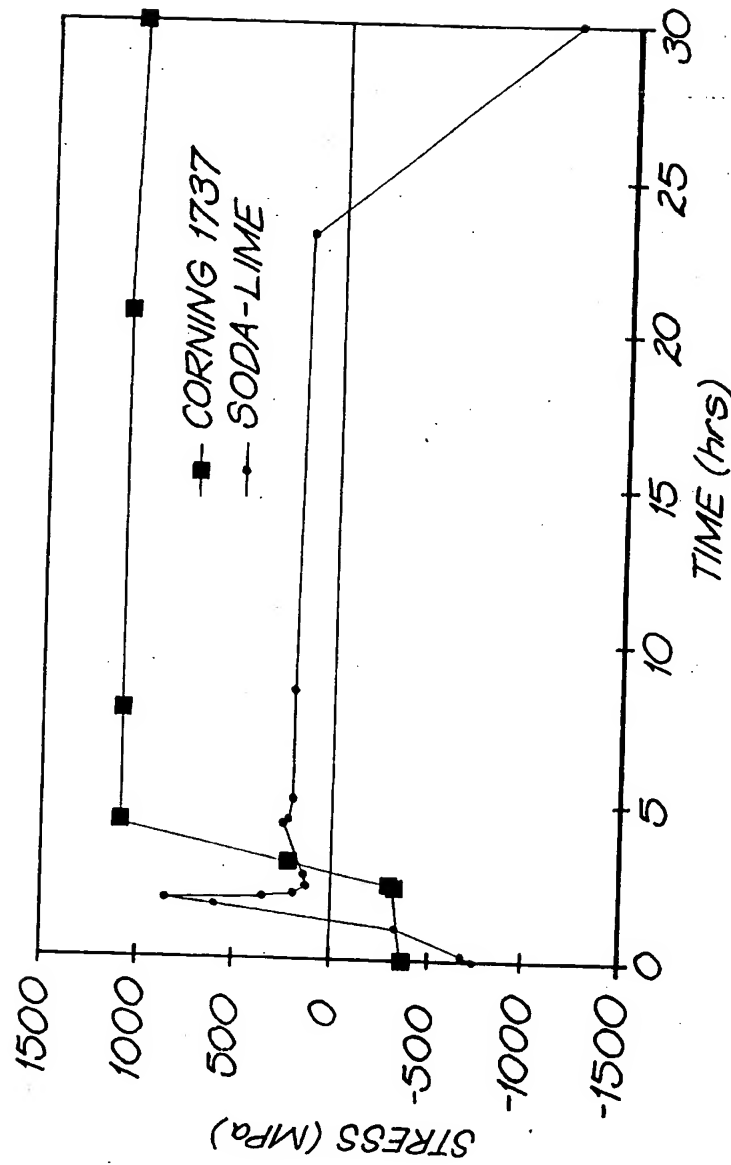
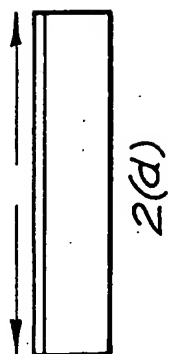
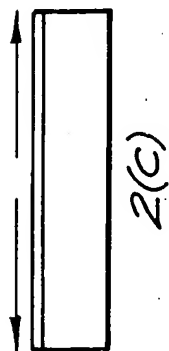


FIG. 1



2(a)



2(b)

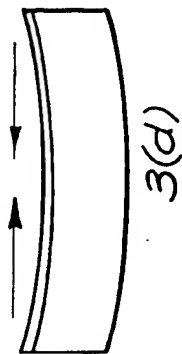


2(c)



2(d)

FIG. 2



3(a)



3(b)

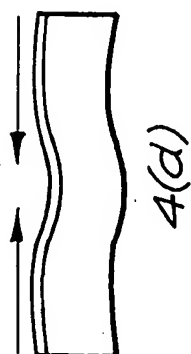


3(c)



3(d)

FIG. 3



4(a)



4(b)



4(c)



4(d)

FIG. 4

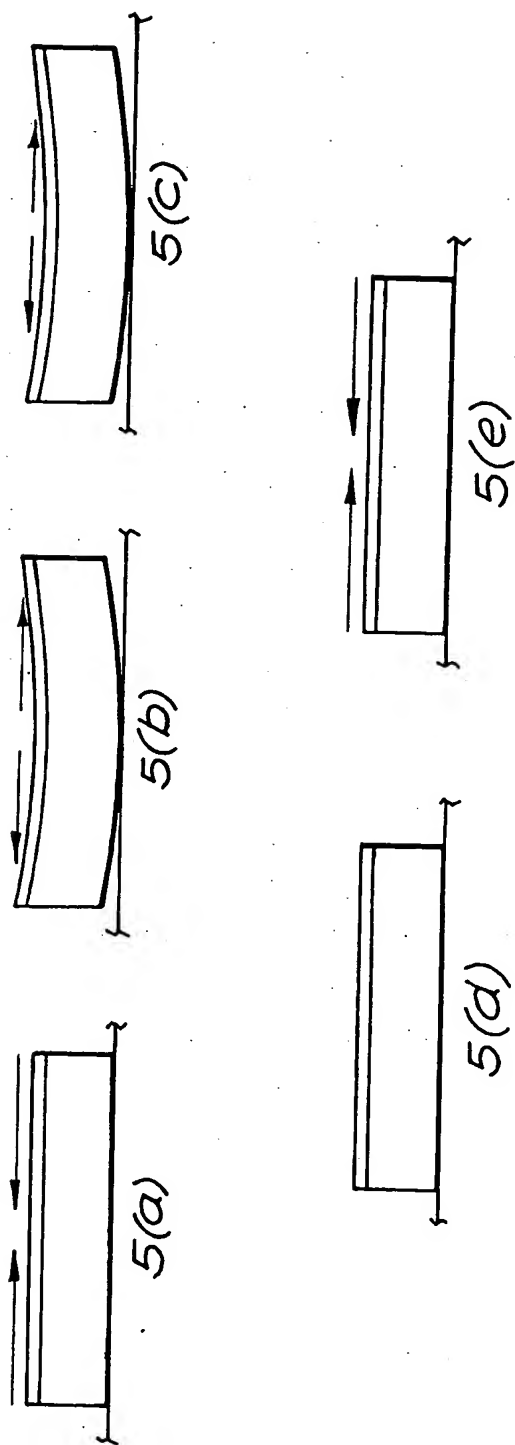


FIG. 5



# INTERNATIONAL SEARCH REPORT

International Application No.

PCT/AU 97/00753

## Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:  
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:  
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. ☐ Claims Nos.:  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a)

## Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

Please see the attached sheet.

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims
2. ☒ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☐ No protest accompanied the payment of additional search fees.

# INTERNATIONAL SEARCH REPORT

International Application No.

PCT/AU 97/00753

## Box II

The intentional application does not comply with the requirements of unity of invention because it does not relate to one invention or a group of inventions so linked as to form a single general inventive concept. In coming to this conclusion the international searching authority has that there are at least two inventions. A comparison of technical features of the independent claims 1, 2 and 4 is presented below:

TECHNICAL FEATURE	CLAIM 1	CLAIM 2	CLAIM 4
A. heating at least the region of the substrate adjacent to the interface between the substrate and the semiconductor material to a temperature above the strain point temperature of the substrate.	YES	YES	NO
B. forming a low strain point temperature intermediate film	NO	NO	YES
C. processing an amorphous semiconductor film	YES	NO	YES
D. depositing an amorphous film	NO	NO	YES
E. depositing a crystalline film	NO	YES	NO
F. cooling the substrate	YES	YES	NO

As can be seen from the above comparison, claims 1 and 2 share a special technical feature A while claim 4 has a special technical feature B. Further, apart from a crystalline semiconductor film on a glass substrate (a well known feature), these claims do not have any common technical feature. Therefore a "technical relationship" between the inventions, as defined in PCT Rule 13.2 does not exist. Accordingly the international application does not relate to one invention or to a single general inventive concept.

# INTERNATIONAL SEARCH REPORT

International Application No.  
PCT/AU 97/00753

## A. CLASSIFICATION OF SUBJECT MATTER

Int Cl<sup>6</sup>: H01L 21/20, 21/84, 31/18, C03C 17/22, C30B 25/00, 28/02, 29/06, 33/02

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC: H01L, C03C, C23C, C30B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

AU: IPC as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPAT, JPAT, USPM: IPC as above with keywords SILICON, STRAIN, GLASS

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	JP 7-109573 A (SEMICONDUCTOR ENERGY LABORATORY CO., LTD.) 25 April 1995 [& US 5674304 A (FUKADA et al) 7 October 1997] Abstract; column 13, lines 10-42 Whole document	1
X	US 5372860 A (FEHLNER et al) 13 December 1994 Column 3, lines 25-53; column 4, lines 36-37; column 6, lines 52-61; claims 1-14	1, 2

☒ Further documents are listed in the  
continuation of Box C

☒ See patent family annex

\* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search  
21 November 1997

Date of mailing of the international search report  
**26 NOV 1997**

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# INTERNATIONAL SEARCH REPORT

International Application No.  
PCT/AU 97/00753

## C (Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	Patent Abstracts of Japan, E-477, page 23, JP 61-203631 A (TOSHIBA CORP) 9 September 1986 Abstract	2
X	Patent Abstracts of Japan, E-703, page 34, JP 63-221610 A (HITACHI LTD) 14 September 1988 Abstract; figure	4
X	Patent Abstracts of Japan, E1470, page 141, JP 5-218367 A (SHARP CORP) 27 August 1993 Abstract; figure	1
X	Patent Abstracts of Japan, E-1037, page 113, JP 2-297923 A (SEIKO EPSON CORP) 10 December 1990 Abstract; figure	2

### Information on patent family members

**PCT/AU 97/00753**

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report		Patent Family Member	
US	5372860	EP	633604
IL	110194	JP	7-140454

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